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Incident and Wake Turbulence and Interactions with Horizontal Axis Rotors.

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Summary:

- HAWTs typically 3 bladed, upwind rotor machines, diameter up to ~150m, tip speed ~ 80+ms⁻¹.
 [HATT prototypes typically 2 bladed, up- & down-stream rotors, diam. ~ 30m, tip speed O(10ms⁻¹).]
- Rotor blades are subject to Random loads due to incident
 Turbulence in the ABL or in wakes of other upstream
 turbines when deployed in farm arrays.
- As part of SuperGen (MAXFARM) Imperial College is investigating aerodynamic control to reduce unsteady blade loading.
- This presentation will deal with some issues of the turbulence impacting the rotor blades.

Rotor Wakes. Wind-Farm (Horns Rev, offshore) Denmark)



Flow Field Computation

- URANS computation of the flow around a (downwind) HAWT. [Acknowledgement F. Zahle (Risoe Lab.)]
- Iso-contours of absolute vorticity shown.
- Tip and root vortices preserved well downstream of turbine when incident flow is uniform.





Aeroelastic Rotor Flow Simulation

[Free Wake Panel Method – unsteady vortex lattice method (UVLM), FEA Beam element dynamics, Twin-bladed rotor].



Mesh for convected turbulence field



INCIDENT TURBULENCE (ABL) Simulated Streamwise Velocity Component assuming von-Karman spectrum and Gaussian probability. Von Karman spectrum u velocity component



Power and Thrust Coefficient Response



 $\Lambda = 5$

INCIDENT TURBULENCE DISTORTION Schematic of Actuator Disc Mean Flow



(Homogeneous) distortion of small length-scale turbulence $\overline{u^2}/\overline{u_{\infty}}^2$, (Batchelor & Proudman, Farr & Hancock)



Spectrum Suu of distorted small length-scale turbulence, ---- undistorted (von Karman spectrum).



Mean square intensity and transverse length-scale of distorted turbulence $\overline{u^2}/\overline{u_0^2}$, $L_2/L_{2,0}$



Distortion of Turbulence into a HAWT Rotor (axis)



Incident Wakes from Upwind Rotors

Mean flow and turbulence

Distortion of mean flow profile of rotor wake.



Mean ΔU on axis at rotor / ΔU_{∞} Velocity defect $\Delta U_{\infty} = 0.25U_{\infty}$

Turbulence and Wake Interactions (Wind Tunnel Expt.)



Wake of a three bladed rotor in uniform incident flow (UVLM free vortex wake)



Mean wake velocity profile U(y), versus experiment of Hancock & Pascheke (o)



Actuator disc or line representation of rotors for RANS computations of turbulence in wind farms.

- Sinks of mean flow momentum.
- Sources of turbulence KE. (κ)
- Length-scale of rotor wake turbulence (ε)

Alternatively LES simulations (eg: Porte-Agel et al.)

Transverse profiles of $\overline{u^2}/U^2$, o Hancock & Pascheke



Spectrum of turbulence in rotor wake 1D downstream of rotor.



Autocorrelation coefficient versus time separation in wake 1D downstream of rotor.



Autocorrelation time-scale L_T in wake of rotor 1D downstream



Turbulence intensity $\overline{u^2}/U_{wind}^2$ versus rotor thrust coefficient C_T

Sampling of turbulent velocities induced in (UVLM) rotor wake indicates a quadratic correlation between $\overline{u^2}/U_{\infty}^2$ and C_T

Turbulence Energy, Length scale and dissipation in rotor wake Approximating $\kappa = \frac{1}{2} \overline{q^2}$ by $\overline{u^2}$

$$L_{\varepsilon} \approx L_{\chi} \sim \frac{(1-a)D}{N_B \Lambda}$$

Therefore dissipation

$$\varepsilon = \kappa^{3/2} / L_{\varepsilon} \sim \frac{N_B \Lambda C_T^3 U_{wind}^3}{(1-a)D}$$

<u>Conclusions</u>

Distortion of turbulence only significant if length scale of turbulence < rotor diameter.

Some distortion (< 15%) of mean wake profiles may be expected.

Some empirical correlations for turbulence KE. (κ) and length-scale (dissipation ε) have been estimated for a rotor wake.