







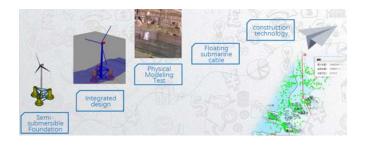






UK&CHN Centre for Offshore Renewable Energy

Joint UK-China Offshore Renewable Energy (ORE) call (2017)



General consideration / Goals and Objectives

The UK – China Offshore Renewable Energy programme aims to develop the next generation of offshore renewable energy (ORE) technologies to enable the safe, secure, cheap and efficient provision of clean energy.

As part of that programme, EPSRC and NERC have co-funded 5 UK-China Projects:

- Resin: Resilient Integrated-Coupled FOW platform design methodology; Lars Johanning (EP/R007519/1)
- FENGBO-WIND: Farming the Environment into the Grid: Big data in Offshore Wind; Mike Graham (EP/R007470/1)
- Extreme wind and wave loads on the next generation of offshore wind turbines; Tom Adcock (EP/R007632/1)
- INNO-MPP: Investigation of the novel challenges of an integrated offshore Multi-Purpose Platform (EP/R007497/1)
- MOD-CORE: Modelling, Optimisation and Design of Conversion for Offshore Renewable Energy (EP/R007756/1)









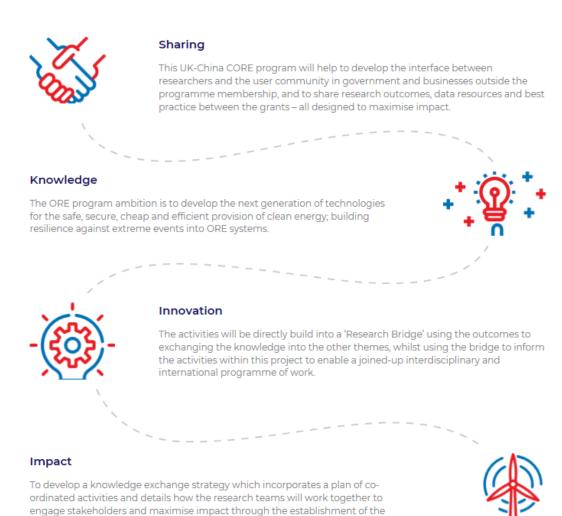








Objectives of UK – China "ORE network"





UK-China CORE programme

UK & CHINA CENTRE FOR OFFSHORE RENEWABLE ENERGY















Engagement activities

Key elements of Engagement plan:

- i) 3 cross-country events,
- ii) Summer Schools,
- iii) Public School engagement,
- iv) (internships), and
- v) (flex funds).



All researchers will hopefully actively engage in this activities enabling a cross-country knowledge exchange and research collaborations.

















UK&CHN | CORE website



info@ukchn-core.com

















Resilient Integrated-Coupled FOW platform design methodology (ResIn)

Prof. Lars JohanningUniversity of Exeter

SUPERGEN Wind General Assembly Dundee, 08th November 2018













China-UK Offshore Renewable Energy

Resilient Integrated-Coupled FOW platform design methodology (ResIn)



Prof. Bing ChenDalian University of Technology





Prof. Lars JohanningUniversity of Exeter















Project Overview

 Aim: "To enhance the design and development of floating offshore renewables, in particular offshore floating wind, as commercially viable electricity infrastructure through a risk based approach allowing building resilience against extreme events."

• Duration: 3 years – 07/2017 – 06/2020











Academic Partners - UK

- University of Exeter (Prof Johanning, Prof Tabor, Prof Pavic, Dr Thies)
 - Hydrodynamic modelling and testing (WP2)
 - CFD modelling (WP3)
 - Structural Reliability assessment (WP4)
- University of Edinburgh (Prof Ingram, Dr Venugopal)
 - Environmental modelling (WP1)
 - CFD coupling (WP3)
- University of Bath (Dr Zang, Dr Blenkinsopp)
 - Particle-In-Cell (PIC) modelling method (WP3)









Academic Partners - China

- Dalian University of Technology (Prof Chen,)
 - Environmental conditions (WP1)
 - OWC damper, Experimental testing (WP2)
 - Hydrodynamic numerical modelling (WP3)
 - Concrete materials (WP4)
- Zheijang University (Dr Zhang)
 - Environmental conditions (WP1)











Industry Partners - UK

- DNV GL
 - Attendance Knowledge Exchange Workshops



- Input through Advisory Meetings
- Review of technical project outcomes (floating platform innovation) to advise on suitable qualification and certification routes with increasing TRL.
- ITPEnergised
 - Participate in Knowledge Exchange Activity
 - Attendance of Industry Forum Workshops
 - Existing contacts/ network in China



Offshore Catapult

- Providing industrial guidance on the scope/outputs (Foundations / sub-structures)
- Participate in Knowledge Exchange Workshop
- Guidance on the Catapult Innovation processes
- Host a postdoctoral researcher for 2 month secondment.













Industry Partners - International

DSA



- Participate in Knowledge Exchange activities
- Guidance on industrial relevance of advanced coupled computational modelling

EDF

- Potential 'end-user' for technology and modelling outcomes
- Participate in Knowledge Exchange activities
- Provide guidance through Advisory













Industry Partners - China

- MingYang Wind Power
 - Participate in Knowledge Exchange activities
 - Offer Innovation Training to their Engineers
 - Participate in Industry Forum workshops
- Shanghai Investigation, Design and Research Institute
 - Participate in Knowledge Exchange activities
 - Participate in Industry Forum workshops





















ResIn - 1st UK-China workshop

10th - 14th November 2017, Dalian University of Technology, Dalian, China

Dalian University of Technology International Convention Center, China, Liaoning Sheng, Dalian Shi, Ganjingzi Qu, 凌工路 2 号















Work Packages

- 1. Enhanced environmental modelling to accurately determine extreme loadings;
- 2. Assessment of novel, porous floating offshore wind structures and active damping mechanisms;
- 3. Enhanced numerical modelling techniques to efficiently calculate the complex coupled behaviour of floating wind turbines;
- 4. Risk based optimisation of designs and engineering implications.

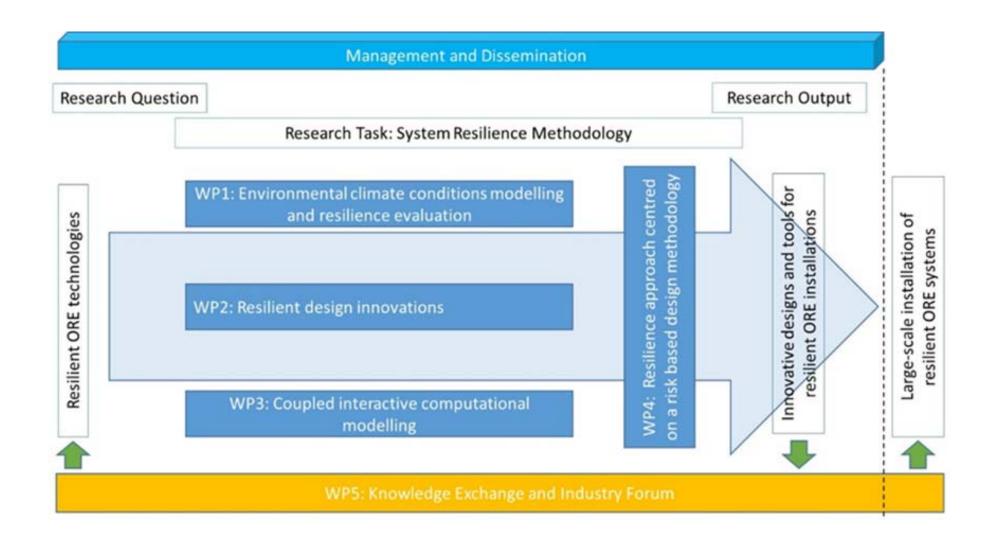




















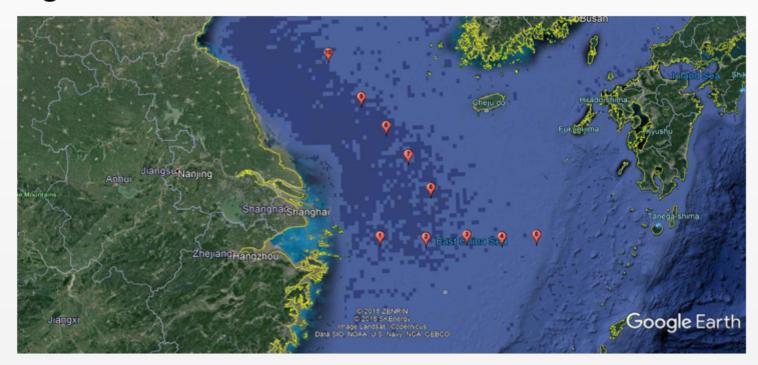




WP1 - Enhanced environmental modelling

Wind analysis

- Calculate return period values using annual maxima method
- PDF fitting













WP2 - Assessment of novel, porous floating offshore wind structures

BEM for mixed solid/porous structures

Integral equations formed in same way for interior and exterior domains:

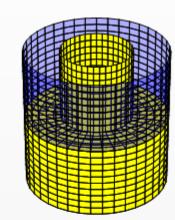
$$2\pi\phi_{j}^{E}(\mathbf{P}) + \int_{S_{E}\cup S_{P}}^{\square} \left(\phi_{j}^{E}(\mathbf{Q}) \frac{\partial G(\mathbf{P}, \mathbf{Q})}{\partial n_{Q}} - G(\mathbf{P}, \mathbf{Q}) \frac{\partial \phi_{j}^{E}(\mathbf{Q})}{\partial n_{Q}}\right) dS = 0$$

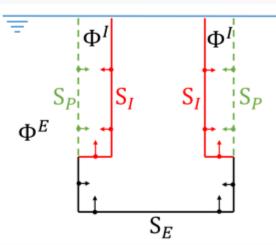
$$-2\pi\phi_j^I(\mathbf{P}) + \int_{S_I \cup S_P}^{\square} \left(\phi_j^I(\mathbf{Q}) \frac{\partial G(\mathbf{P}, \mathbf{Q})}{\partial n_Q} - G(\mathbf{P}, \mathbf{Q}) \frac{\partial \phi_j^I(\mathbf{Q})}{\partial n_Q}\right) dS = 0$$

Boundary condition on porous panels assumes linear pressure-velocity relationship:

$$\frac{\partial \phi_j^E(\mathbf{Q})}{\partial n_O} = \frac{\partial \phi_j^I(\mathbf{Q})}{\partial n_O} = n_j - i\sigma(\phi_j^E - \phi_j^I)$$

 Equations can be discretized in same way, but matrices must be rearranged to account for coupling of inner and outer domains via damping relation.







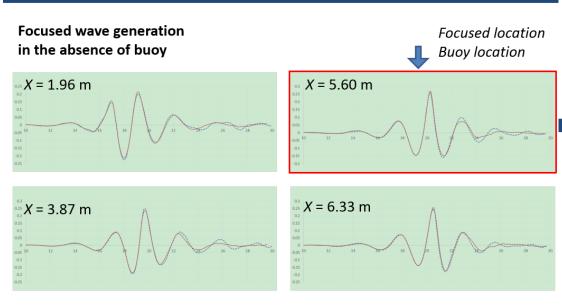






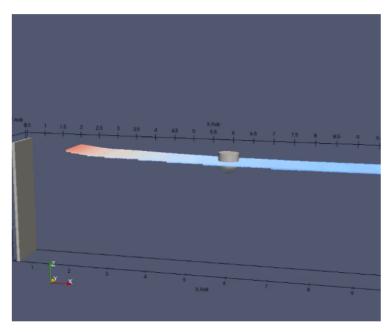


WP3 - Enhanced numerical modelling



Dashed line: experiment; Solid line: numerical

Wave-structure interaction











Static +

6.9 - 12

2.5 - 6.5

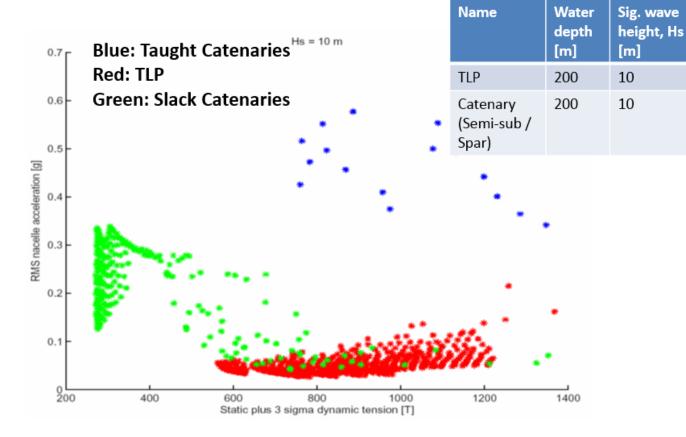
Dynamic

tension [MN]



WP4 - Risk based optimisation of designs

Design Load estimation







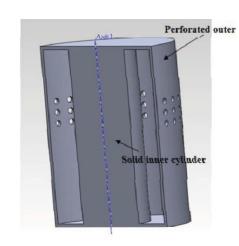






Why porous structures?

- Reduce wave loads on floating platform
- Increase motion damping
 - ▶ Reduce platform motions
 - → Reduce energy loss from turbine
 - → Reduce fatigue damage on structure and drivetrain
 - ► Reduce mooring loads









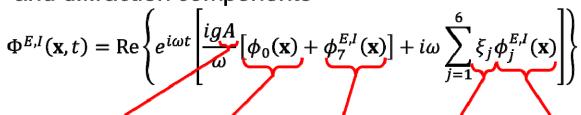






Problem formulation

- Fluid divided into internal/external domains.
- Standard decomposition of potential into radiation and diffraction components



Wave amplitude

Incident potential

Scattered potential

Motion amplitude

Radiation potential









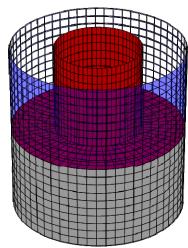


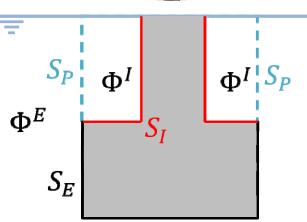




Boundary conditions

- Standard boundary conditions on free-surface, sea bed and solid surfaces, S_E , S_I
- Additional boundary condition on porous surface, S_P:
 - $_{\circ}$ Continuity of velocity: $\frac{\partial \phi_{j}^{E}}{\partial n} = \frac{\partial \phi_{j}^{I}}{\partial n}$
 - o Pressure drop: $\frac{\partial \phi_j^E}{\partial n} = n_j i\sigma (\phi_j^E \phi_j^I)$
 - n_i = normal velocity of surface in j^{th} mode
 - σ = porosity coefficient (0 if solid, ∞ if no porous wall)















Viscous loss:

significant at

low Re

Pressure loss at porous boundary

$$\frac{\Delta P}{\rho} = \frac{\nu}{l} U_n + \frac{C_f}{2} U_n |U_n| + L \frac{\partial U_n}{\partial t}$$

- ΔP = pressure drop
- ρ = fluid density
- ν = kinematic viscosity
- U_n = velocity normal to porous boundary
- l = friction coefficient (dimension length)
- C_f = dissipation coefficient (dimensionless)
- L = added mass coefficient (dimension length)

Turbulent dissipation: significant at high Re

Added mass: Dependent on size of openings



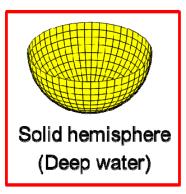


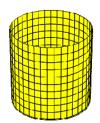




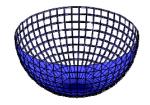


Verification and validation of BEM model

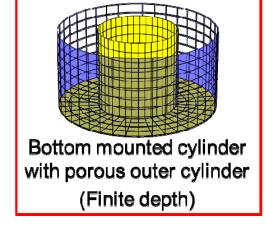


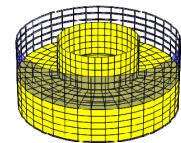


Bottom mounted cylinder (Finite depth)



Porous hemisphere (Deep water)





Truncated cylinder with porous outer cylinder (Deep water)





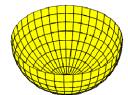


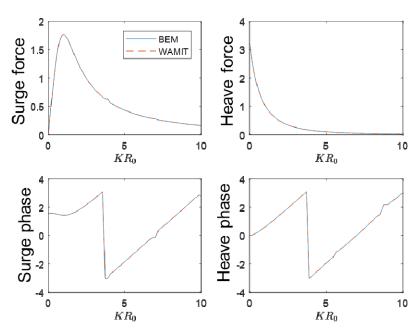




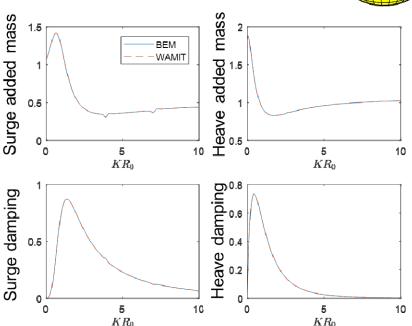
Numerical Comparison via WAMIT

Solid hemisphere (deep water)





Non-dimensional excitation force vs. non-dimensional frequency



Non-dimensional added mass and radiation damping





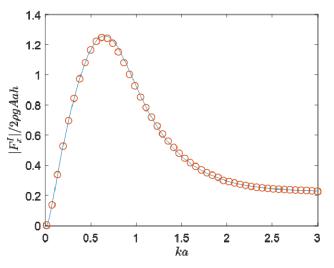




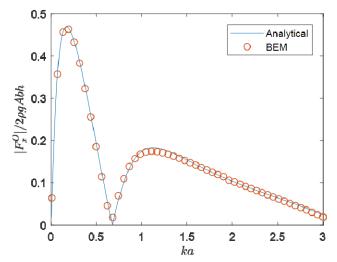


Numerical Comparison via Analytic model: Wang & Ren (1994)

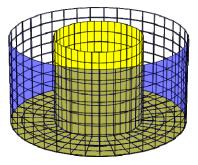
Concentric cylinder (finite depth)



Non-dimensional surge force on inner cylinder



Non-dimensional surge force on outer cylinder



Water depth = h
Inner radius = a = h
Outer radius = b = 2h
Porosity coef. G = 2











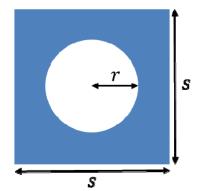
Experimental Comparison

Tank tests at DUT, China

- Porous cylinder with / without solid inner cylinder
- Solid cylinder Ø250mm
- Porous cylinders Ø375, 500, 750mm
- Water depth h = 1 m
- Porosities $\tau = 0.1, 0.2, 0.3$
- 300 tests (29 regular waves, 4 irregular waves)







Porosity
$$\tau = \frac{\pi r^2}{s^2}$$





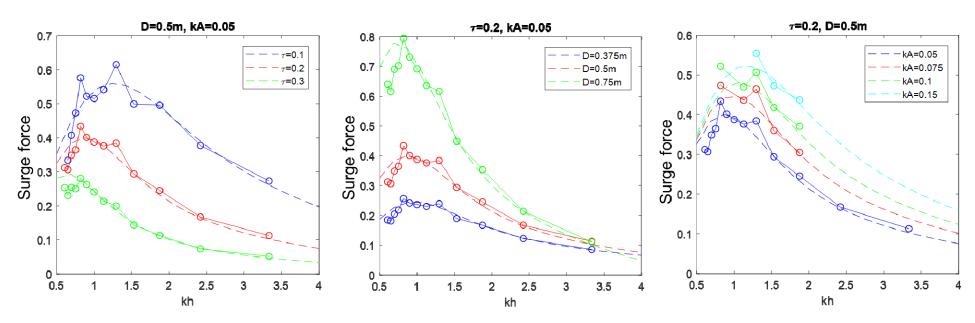






Experimental Comparison

Validation against tank tests (outer cylinder only)



Non-dim. surge force vs non-dim. frequency

Circles: experimental. Dashed lines: numerical





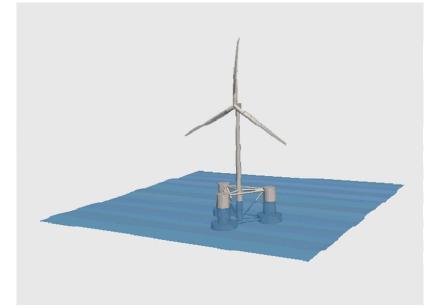


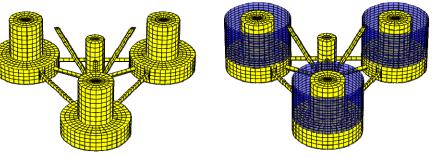




Next steps

- Numerical investigations into effect of porous shroud in terms of:
 - Excitation force
 - o Added mass & damping
 - Mean drift force
 - Motion RAOs
- Tests at FloWave & DUT to validate numerical predictions







Resin Publication to date





Journal papers:

- C. Yang, Y. Wang, S. Weller, De-Zhi Ning, L. Johanning; (2018). Experimental and numerical investigation on coupled motion characteristics of a tunnel element suspended from a twin-barge; Ocean Engineering 153 (2018) 201–214, doi: 10.1016/j.oceaneng.2018.01.112
- Mackay E, Johanning L. (2018) A generalised equivalent storm model for long-term statistics of oceanwaves, Coastal Engineering, volume 140, pages 411-428, DOI:10.1016/j.coastaleng.2018.06.001.
- E. Mackay, L. Johanning (2018) Long-term distributions of individual wave and crest heights, Ocean Engineering, volume 165, pages 164-183, DOI:10.1016/j.oceaneng.2018.07.047.
- E.B.L. Mackay. "Approximation of the free-surface Green function in finite depth" J. Eng. (Math. (Submitted)

Conference papers:

- E. Mackay, L. Johanning. (2018) A Simple and Robust Method for Calculating Return Periods of Ocean Waves. Proceedings of the ASME 2018 37th International Conference on Ocean, Offshore and Arctic Engineering, OMAE2018, June 17-22, 2018, Madrid, Spain.
- E. Mackay, A. Feichtner, R. Smith, P.R. Thies, L. Johanning. (2018) Verification of a Boundary Element Model for Wave Forces on Structures with Porous Elements. RENEW 2018, 3rd International Conference on Renewable Energies Offshore, 8 10 October 2018, Lisbon, Portugal.















Thank you for listening - Questions



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Dezhi NING
Jun CHANG
Haigui KANG
Wei SHI
Dahai ZHANG
Dongsheng QIAO

Niankin REN` Hai/DU /

















