Scottish University of the Year 2017





School of Science and Engineering University of Dundee

Investigating installation requirements for optimised screw piled jacket foundations

SUPERGEN Wind General Assembly

Dr Michael Brown

Thursday 27 April 2017



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Overview

- \rightarrow Background to screw piles and the deployment challenge
- \rightarrow Current screw pile design elements and performance
- → Progress in Physical Modelling
- \rightarrow New design methods and Optimisation
- \rightarrow Numerical Modelling progress
- \rightarrow Field testing to verify our work
- \rightarrow Outputs and opportunities

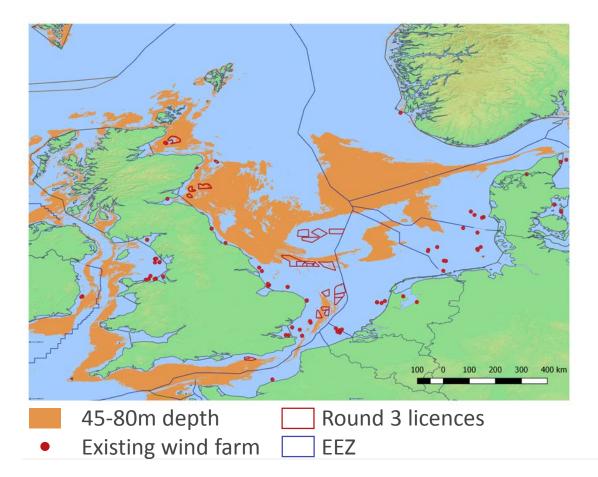


Lego Mindstorm public engagement

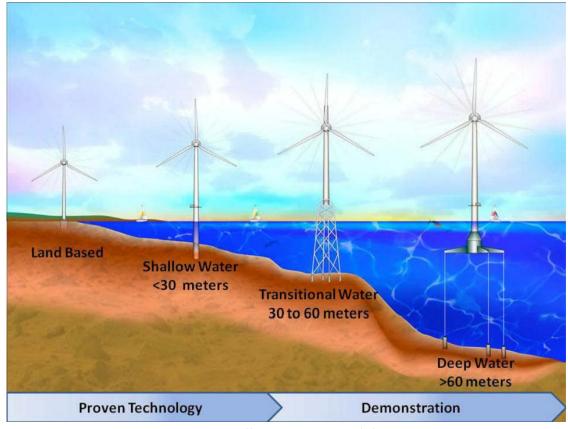
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Screw piles for wind energy foundation systems: Deployment challenge

 \rightarrow Offshore wind is advancing in to deeper water



→ Foundation system required for intermediate depths between monopile and floating

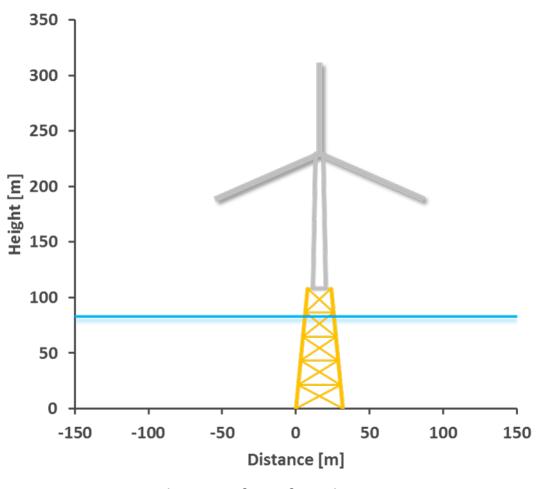


By Jplourde umaine - Own work, CC BY-SA 4.0, https://commons.wikimedia.org/w/index.php?curid=49937716



Screw piles for wind energy foundation systems: Deployment challenge

- \rightarrow Offshore wind is advancing in to deeper water
- → Foundation/support systems required for intermediate depths between monopile and floating
- → Systems may create increased foundation operation events (4 piles per jacket)
- → Concern/regulations associated with noise from piling (continuous long term installation events)
- → Cost effective solution required (20-30% cost)
- \rightarrow Jacket structures supported on screw piles?

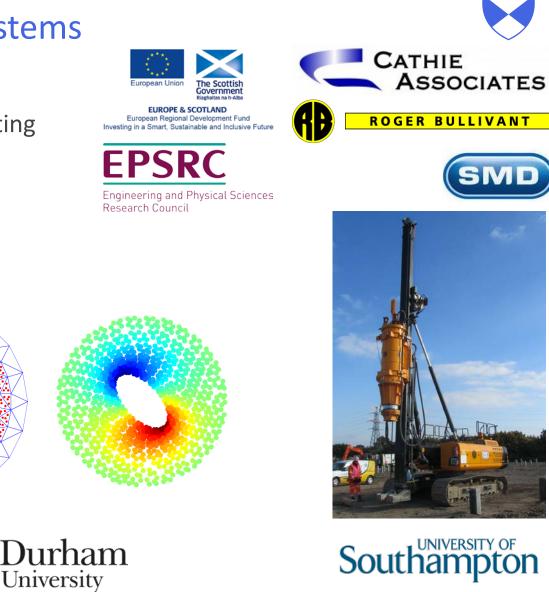


Visual output from foundation optimisation spreadsheet (80m water depth)

Screw piles for wind energy foundation systems

- → Physical modelling, numerical modelling, field scale testing
- \rightarrow Investigate optimised design solutions
- → Improved design methods for future implementation

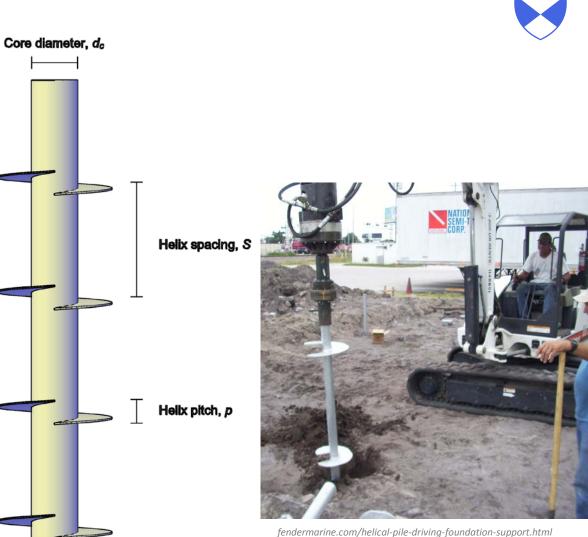






Introduction to Screw Piles

- Tubular steel core/shaft \rightarrow
- Single/multiple helical plates \rightarrow
- Helices regularly spaced (generally) \rightarrow
- Many uses: \rightarrow
 - Historically offshore: Maplin Sands Lighthouse \rightarrow (1838)
 - Contemporary use typically onshore \rightarrow
 - \rightarrow Pylons, guy lines, underpinning...
- Benefits over straight-shafted pile: \rightarrow
 - Improved axial capacity (soil-soil shear) \rightarrow
 - Lower installation noise & vibration than driven \rightarrow



Helix diameter, D_h

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Screw pile design considerations: How big is an offshore screw pile?



- → Up-scale screw piles from typical onshore designs to manage offshore loads / BMs
- \rightarrow Principle influential factors include:
 - \rightarrow Loading
 - $\rightarrow~$ Wind / waves / water depth / turbine /
 - \rightarrow Soil properties
 - → Screw pile geometry (upscaled)
- → Challenge to meet installation torque requirements (or predict)

Typical onshore use



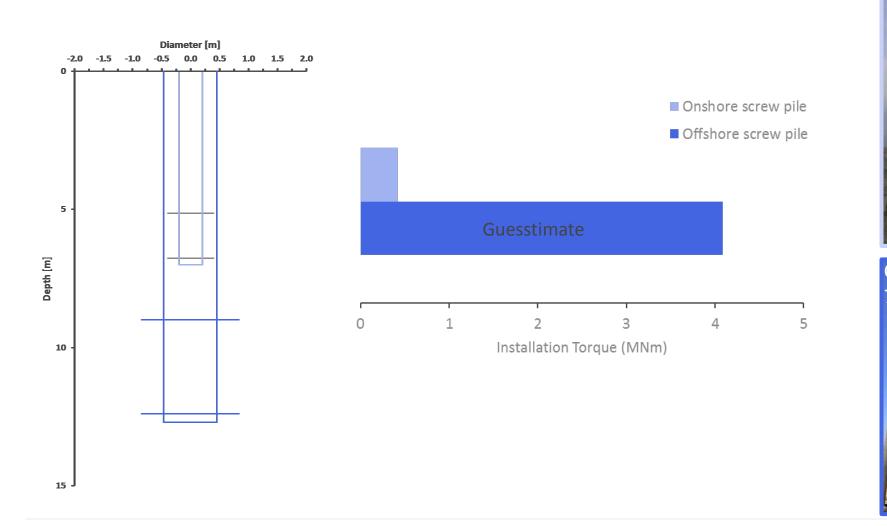
Offshore jacket installation (driven piling)



slpconsult.com/news.html?newsId=20

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Installation Torque required for offshore deployment?





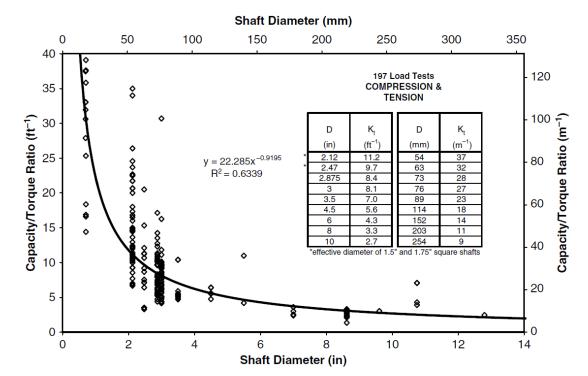
Largest torque head 490 kNm!





Existing screw pile design methods: Capacity & Torque

- \rightarrow Empirical methods
 - \rightarrow Hoyt and Clemence (1989), Perko (2009)
 - \rightarrow Correlates installation torque to axial capacity
 - → Based on database of "small" onshore piles
- \rightarrow Problems?
 - → Correlating torque and capacity reliant on control (how big are the crowding forces?)
 - → Torque used to verify installed capacity not predict torque
 - → Effect of changing geometry not clear for capacity and torque.

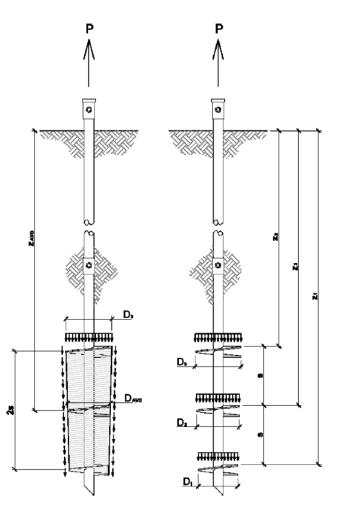


PERKO, H. A. (2009) Helical piles: a practical guide to design and installation, Hoboken, New Jersey, John Wiley & Sons.



Existing screw pile design methods: Capacity

- \rightarrow Empirical methods
 - \rightarrow Hoyt and Clemence (1989), Perko (2009)
 - \rightarrow Correlates installation torque to axial capacity
 - \rightarrow Based on database of "small" onshore piles
- → Analytical methods (semi-empirical)
 - $\rightarrow~$ Analyses shear and bearing resistances
 - → Assumes individual plates or trapped sand column (soil-soil shear)
- \rightarrow Problems
 - \rightarrow When does mechanism change (S/D_h, D_h/D_c, D_r)?



PERKO, H. A. (2009) Helical piles: a practical guide to design and installation, Hoboken, New Jersey, John Wiley & Sons.

Existing screw pile design methods: in service capacity

- \rightarrow Empirical methods
 - \rightarrow Hoyt and Clemence (1989), Perko (2009)
 - \rightarrow Correlates installation torque to axial capacity
 - \rightarrow Based on database of "small" onshore piles
- → Analytical methods (semi-empirical)
 - \rightarrow Analyses shear and bearing resistances
- \rightarrow CPT Common Site Investigation tool
 - → Relates screw pile capacity to CPT cone and shaft resistances
- \rightarrow Problems
 - \rightarrow Highly empirical (alpha x q_c)
 - → Onshore small pile experience

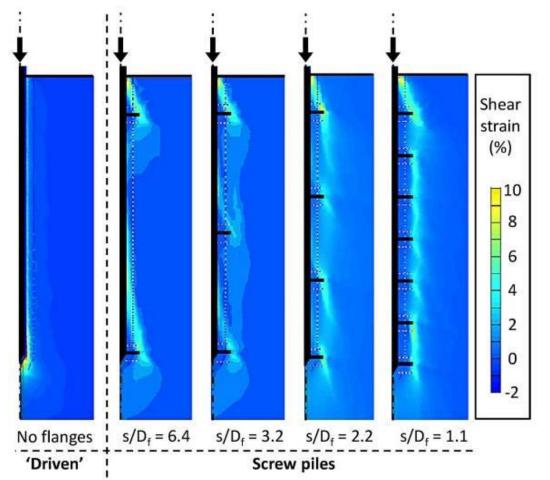


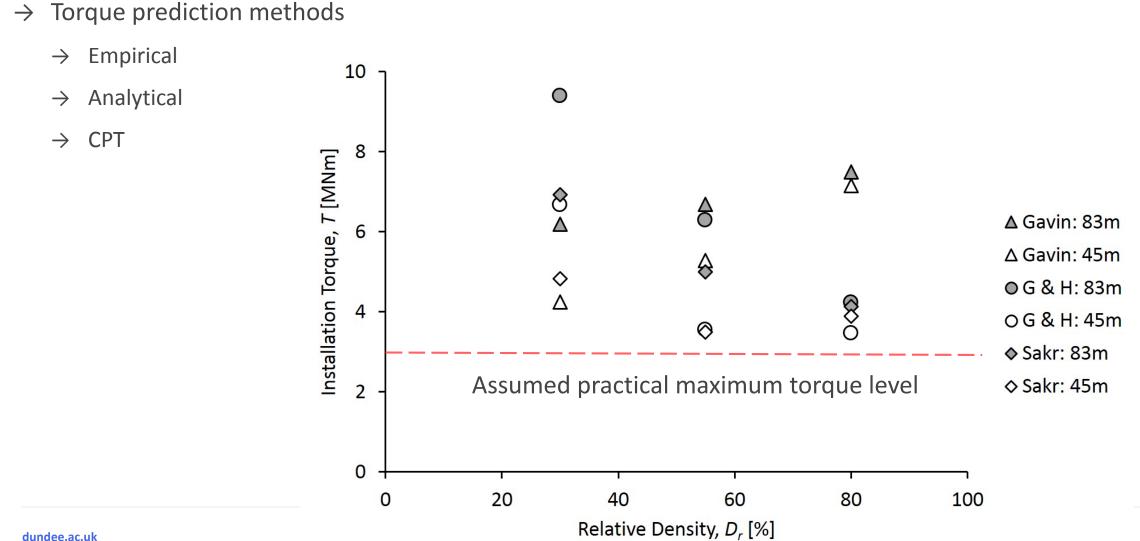




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- $\rightarrow~$ CPT Common Site Investigation tool
 - → Relates screw pile capacity to CPT cone and shaft resistances
- \rightarrow Standard Numerical modelling (S/D_h, D_h/D_c)
- \rightarrow Problems
 - \rightarrow Generally unable to model installation effects
 - \rightarrow Needs model or field verification





Existing screw pile design methods: Existing installation torque prediction?

 \rightarrow





Development of centrifuge test equipment at UoD

- → 2D actuator system for centrifuge modelling (Vertical and rotational servo actuator system)
- \rightarrow Allows installation and testing in single in-flight operation (50th scale or 50g)

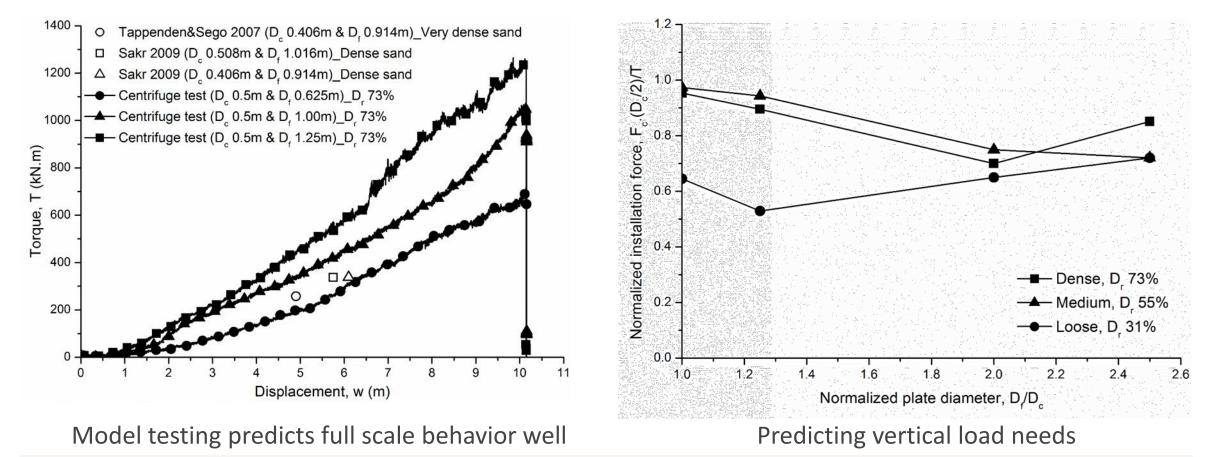


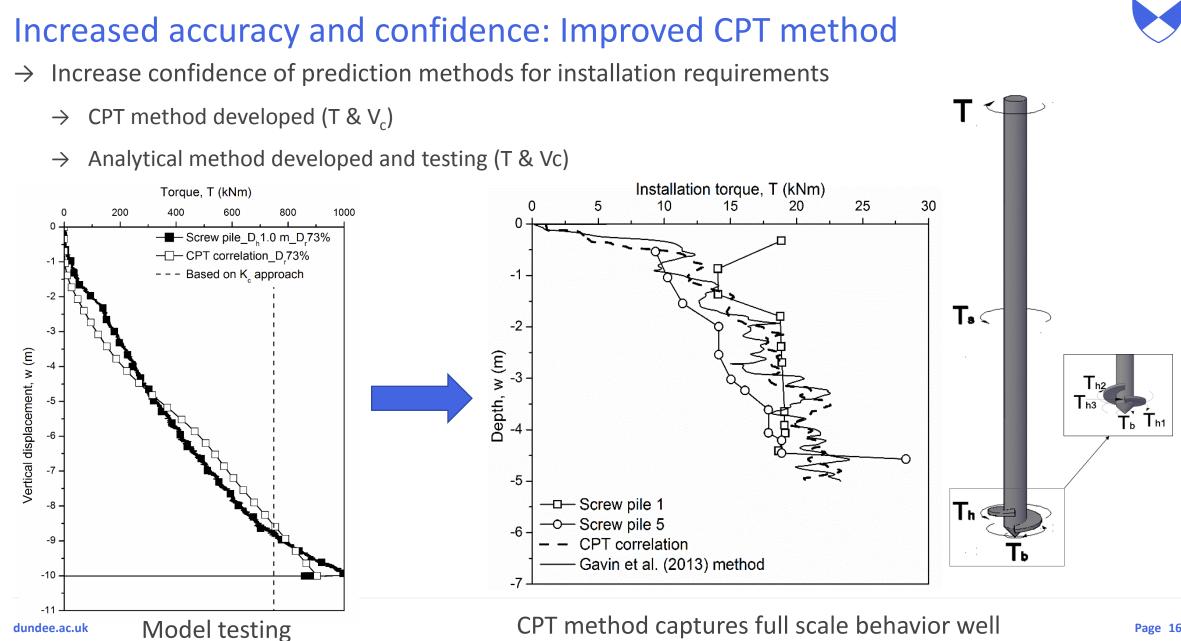




Centrifuge testing at UoD: Scaled up but non-optimised geometry

Preliminary centrifuge test results: Insights into installation requirements





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CPT method captures full scale behavior well



Optimised design

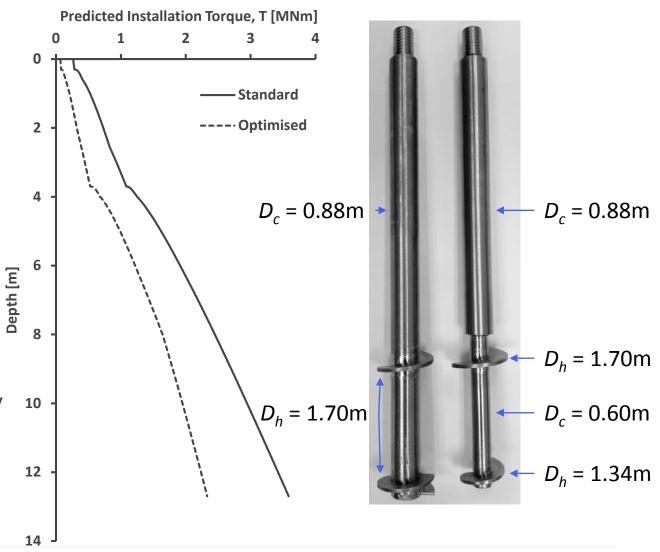
- → Optimised designs required to reduce installation requirements
 - \rightarrow Reduce dimensions where possible
 - \rightarrow Helix diameter
 - \rightarrow Core diameter
- \rightarrow Investigate with centrifuge tests
 - \rightarrow Check prediction methods
 - \rightarrow Check capacity as anticipated

Durham

University

→ Check sensitivity of torque reduction to geometry change

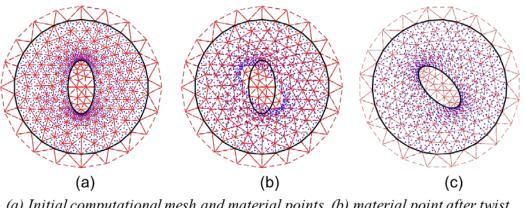
Southampton





- → Finite Element Analysis (FEA) cannot model large scale deformation (Screw piles). 10-20m?
- → Numerical modelling advantages in predicting effects of geometry changes/efficient (S/D_f)
- → Material Point Method (MPM) can model effects of screw pile installation on soil body
- \rightarrow Key components of DU approach
 - → Moving mesh for displacement boundary conditions
 - → elasto-plastic material models for both soil and interface
- → Plan to map changes on soil from MPM on to standard FE as starting point. MPM to captures installation phase.

Moving mesh: a mesh always conforming with the boundary of the deformed body.



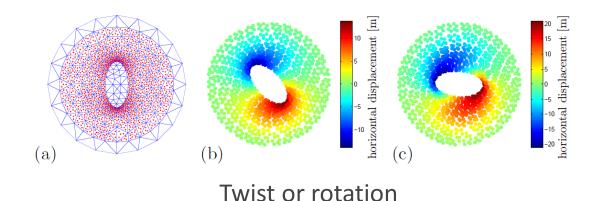
(a) Initial computational mesh and material points, (b) material point after twist 45° without moving mesh, (c) material point with moving mesh

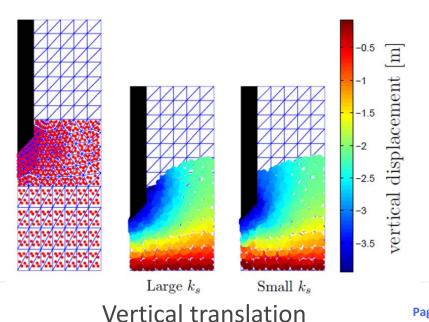
Screw pile twists and penetrates over large distances

Durham University

Numerical modelling: Progress to date

- Decomposed the to rotation and translation, and \rightarrow developed codes for 2D modelling of motions
- The standard MPM and several advanced \rightarrow extensions investigated to identify optimal for modelling strategy
- Strategies for accuracy and stability determined: \rightarrow
 - non-uniform triangular mesh \rightarrow
 - implicit implementation \rightarrow
 - convected particle domain interpolation \rightarrow
 - finite-volume particle domains for quadrature \rightarrow
- Next step: Combine methods used in 2D models to \rightarrow develop the 3D model



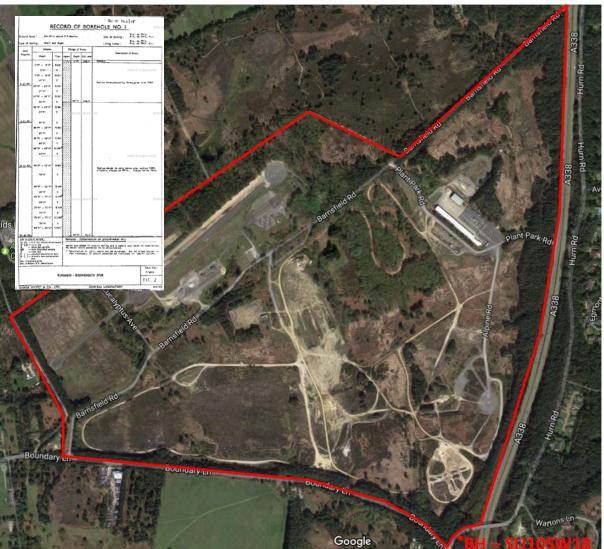


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Field testing: Identifying field study test sites. Southampton

- → Working with Roger Bullivant (RBL) to identify suitable test sites and design field tests.
- → Desk study carried out on the feasibility of two sites proposed by RBL - Sommerford Keynes and Warmell Quarry.
 - → Sites ruled out due to unsuitable ground conditions
- → QinetiQ's Hurn proving ground identified as a possible sand test site
 - → Military vehicle test site (25km from UoS)
 - → Substantial supporting facilities
 - \rightarrow Promising ground conditions
 - → Potential to become a national sand field study resource?
- \rightarrow In discussions with with QinetiQ and In Situ SI dundee.ac.uk





Field testing: Designing equipment & Field tests

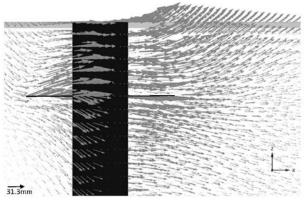
- → Field test design and model testing has identified need for specialist instrumentation
 - → UoD work feeding into design of a bespoke wireless combined torque-load cell
 - → RBL interested in potential for existing CFA piling rig fleet in UK
- → UoS to design field piles and installation equipment based upon coming UoD testing
 - \rightarrow Access to site required to characterise soil (CPT)
 - → Ordering and fabrication of piles based upon UoD findings and suggestions.





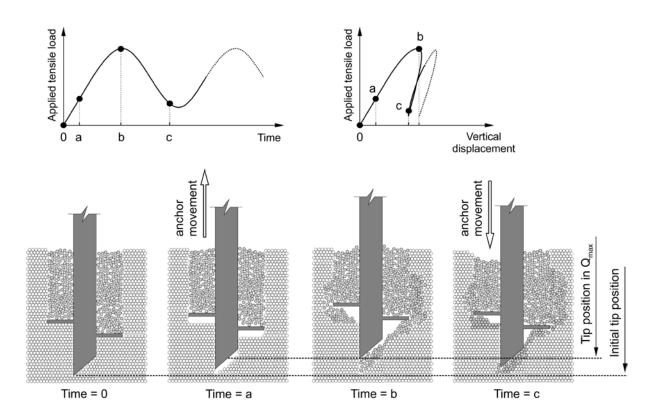
Some questions to tackle as the project progresses

- → Expanding the prediction of installation behaviour to in service performance
- \rightarrow Cyclic performance
- \rightarrow Behaviour in other soil types
- → Lateral screw pile behaviour and performance



(b) D_p =750mm (Flange at 1.0mbgl)

FE Modelling of a laterally loaded screw pile (Al Baghadadi et al 2015)



Tensile cyclic loading of a single plate screw pile (Schiavon et al 2017)

Some outputs and Opportunities

- → 2017- Euro 195k H2020 Fellowship: Screw anchors for floating ORE (2 year fellowship), UoD.
- \rightarrow 2017- £1.25M EPSRC WindAfrica, DU
- \rightarrow EPSRC ORE China bid submitted, DU & UoD + BGS
- → 2017- £220k Forthwind Demonstration Project. 2B Energ



Screw piles engage with school children at Lego Mindstorm dundee.ac.uk



Effects of vertical loading on lateral screw pile performance

 Therar A. Al-Baghdadi BSc, MSc PhD Cancidate, Civil Engineering, University of Dundee, Dundee, Scotland (corresponding author: Lalbaghdadi@dundee.ac.uk)
 Michael J. Brown BEna, PhD

Reader, Civil Engineering, University of Dundee, Dundee, Scotland

- Jonathan A. Knappett MEng, PhD
- Reader, Civil Engineering, University of Dundee, Dundee, Scotland
 Asad H. Al-Defae BSc, MSc, PhD
- Research Associate, Civil Engineering, University of Dundee, Dundee, Scotland



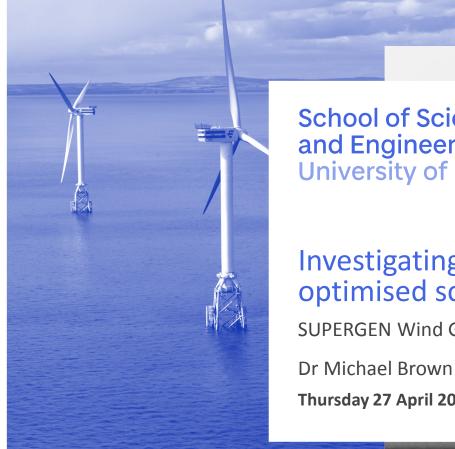
The offshore wind energy sector faces new challenges as it moves into deeper water deployment. To meet these challenges, new and efficient foundation solutions are required. One potential solution is to upscale onshore screw piles but they require verification of performance for new geometries and demanding loading regimes. This paper presents a three-dimensional finite-element analysis investigation of screw pile behaviour when subjected to combined vertical and lateral loading in sand. In the investigation, the screw pile length and helical plate diameter were varied on piles with a fixed core diameter while subjecting the piles to combined axial and lateral loading. The results were compared with results from straight shafted piles with the same core diameter. The results of the analysis revealed that vertical compression loads increased the lateral capacity of the screw piles whereas vertical uplift loads marginally reduced the lateral capacity. The downside of this enhanced lateral capacity is that the screw piles experience higher bending moments. This suggests that, when using screw piles for offshore foundation applications, structures should be designed to maintain axial compressive loads on the piles and induced bending moments and to be advantable accessed when deviding on anyonista structurel certions

First journal paper published



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